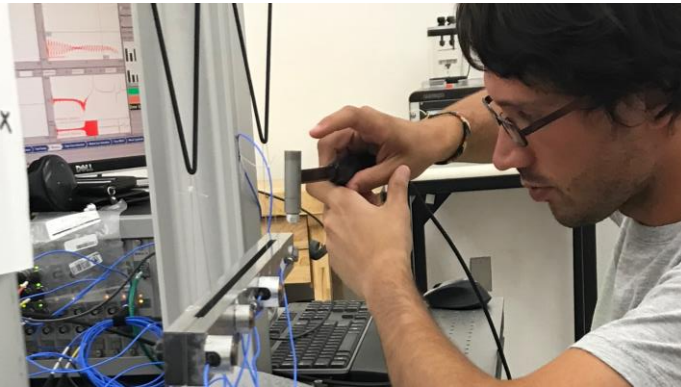
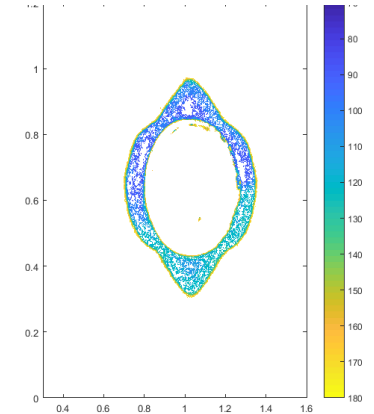
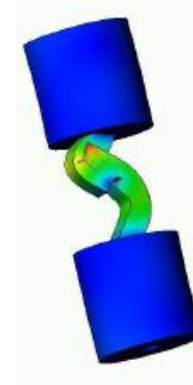


Exceptional service in the national interest



N=O=MAD

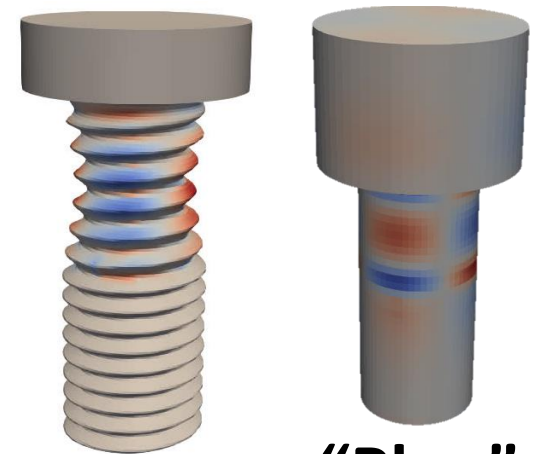
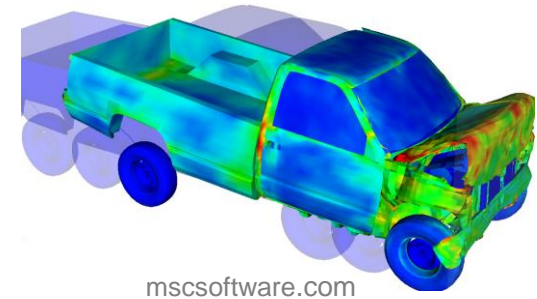
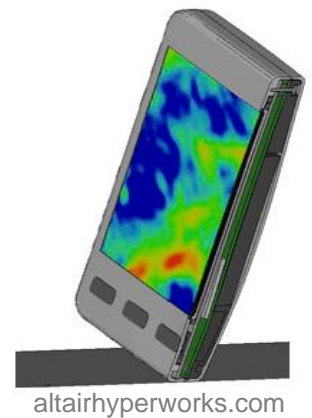


Constructing Optimal Surrogate Models for Bolted Fasteners in Multiaxial Loading

Ernesto Camarena, Anthony Quintana, Victoria Yim

Introduction

- Simulations of structural systems in adverse environments
- Prohibitive computational burden of hundreds of fasteners
- Enormous length scale differences
 - System size, $O(1e3 \text{ mm})$
 - Bolt size, $O(100 \text{ mm})$
 - Thread size, $O(1 \text{ mm})$
- Common fastener modeling
 - So-called “Plug”
 - Analysts rely on pure tension data: no other load angles



“Plug”

Motivation

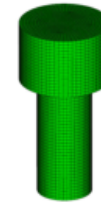
- Research questions:
 - How well do plug models work for an arbitrary loading pull direction?
 - How can plug modeling be modified to improve predictive behavior?
- Solution--Compare plug model to:
 - Experiment data at various load pulls
 - A fully threaded FE model



Methodology: Overview

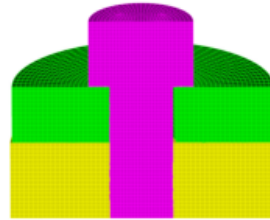
Calibrate Numerical Hardening Curve to Experiments

- Implicit solve, no contact
- 0° load angle (tension only)



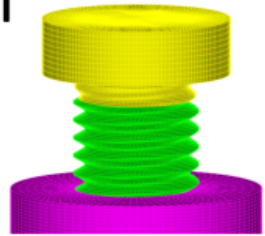
Numerical Plug Model

- Explicit w/ contact
- 0°, 30°, 60°, 90° cases
- Compare w/ experiments @ SNL



Numerical Threaded Model

- Explicit w/ contact
- 0°, 30°, 60°, 90° cases
- Compare w/ experiments @ SNL

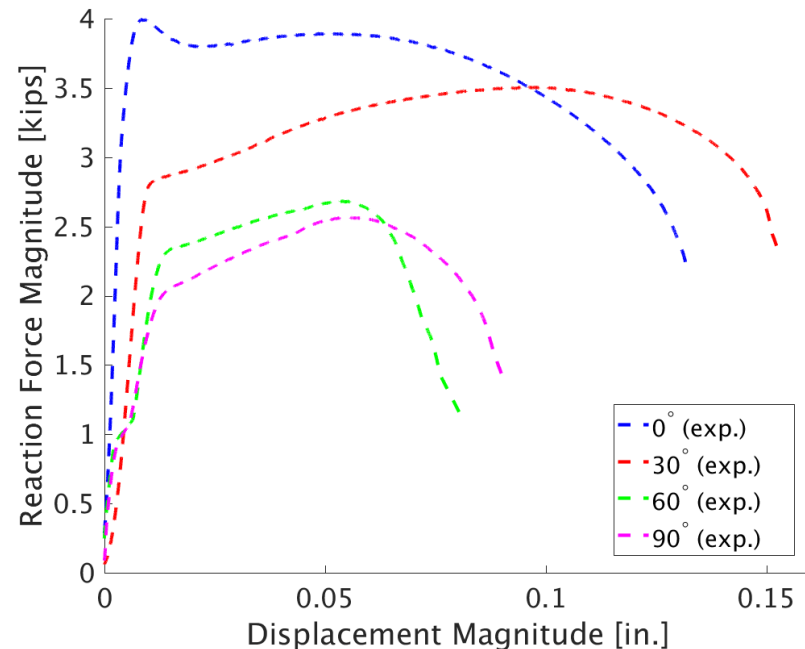
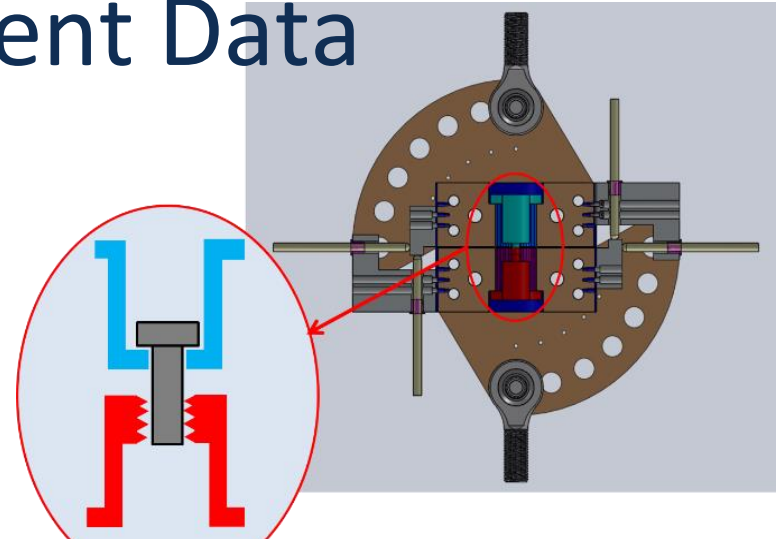
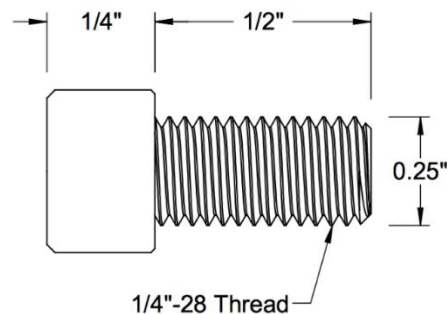


Compare Plug vs. Threaded Model

- 0°, 30°, 60°, 90° cases

Methodology: Experiment Data

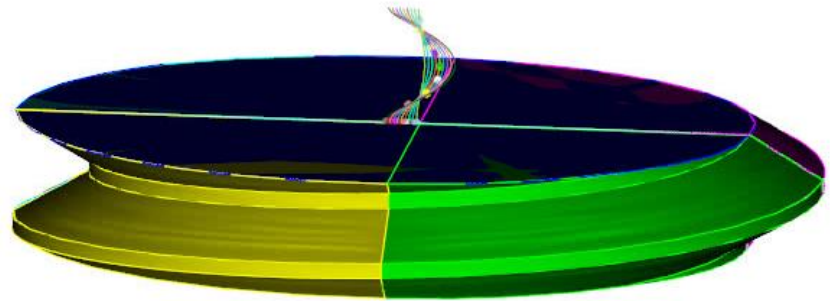
- Multiaxial fastener test setup
 - Setup allows for displacing at various angles
- Fastener details:
 - 18-8 Stainless steel
 - UNF thread type



Methodology: Geometry and Mesh

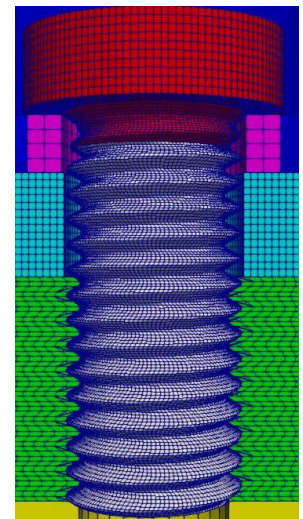
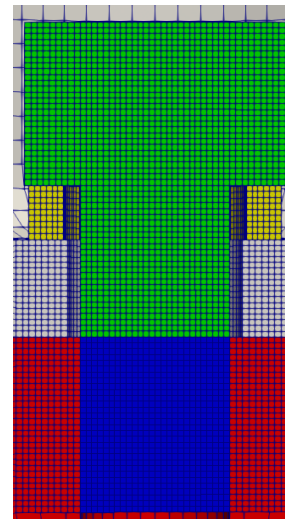
■ Geometry

- Plug uses relatively simple geometry
 - Tensile stress radius
- Threaded model created in slices along helix
 - Fully 3D model



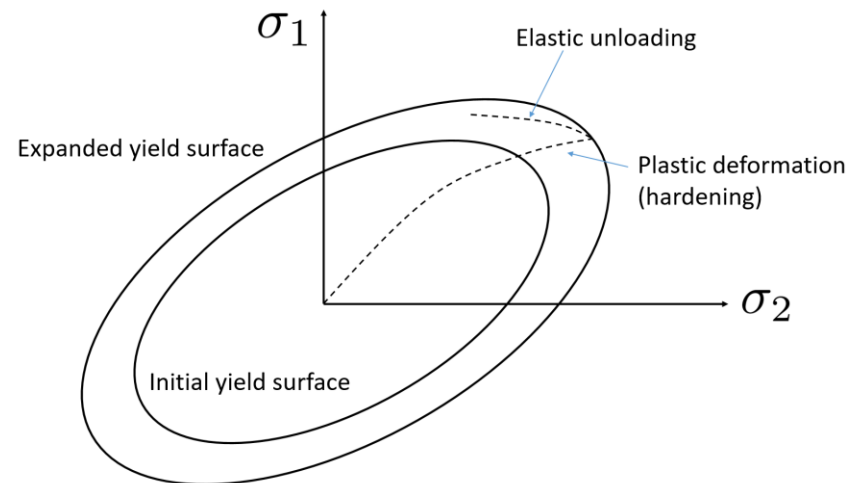
■ Mesh

- Refined regions near fastener
- Coarse mesh for upper and bottom bushing



Methodology: Constitutive Model

- Elasticity: Young's Modulus = 30e6 psi, Poisson's Ratio= 0.3
- Plasticity
 - Isotropic Hardening
 - Multi-linear elastic-plastic hardening curve
 - Yield stress = 93e3 psi
 - Yield Surface retains its shape and is symmetric about the origin
 - Increases uniformly as the material deforms plastically
 - Rate independent



Methodology: Failure Criteria

- Hardening Curve Definition: Multi Linear Elastic-Plastic (MLEP)
 - Linear piecewise hardening curve defined with discrete pairs of equivalent plastic strain (EQPS) and yield stress.

$$D_{ij} = D_{ij}^e + D_{ij}^p$$

- Failure Models
 - Element death based on EQPS limit.
 - Ductile Failure Model (ml_ep_fail)
 - Failure in a given element initiates when its tearing parameter (t_p) reaches a critical value. The element stiffness then decreases with increasing crack opening strain (strain in the direction of the max principal stress).

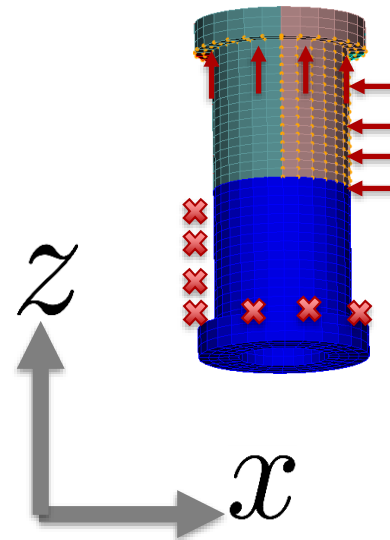
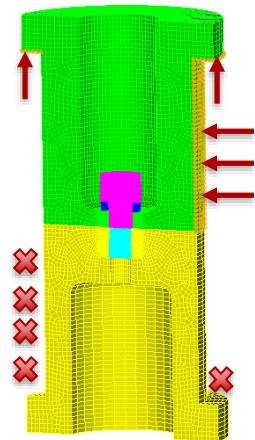
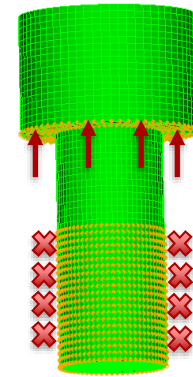
Methodology: Boundary Conditions

- Basic Plug

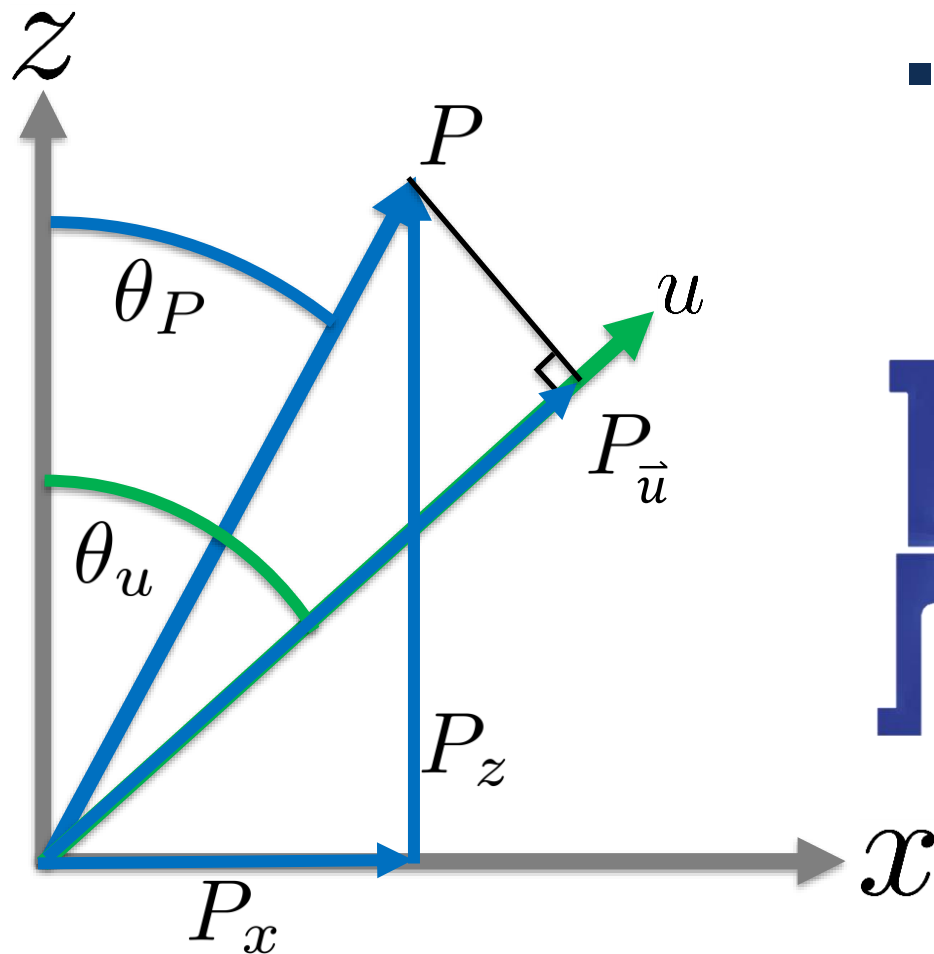
- 0° case: only +z displacement

- Plug with Bushings & Threaded Model

- 0° case:
 - Displace +z face of upper bushing
 - Fixed lower z face of bottom bushing
- 30° , 60° , and 90° case:
 - Displace +x face of upper bushing
 - Displace +z face of upper bushing
 - Fixed lower -x face of bottom bushing
 - Fixed lower z face of bottom bushing



Methodology: Post-Processing



- Load projection

- 30° & 60°

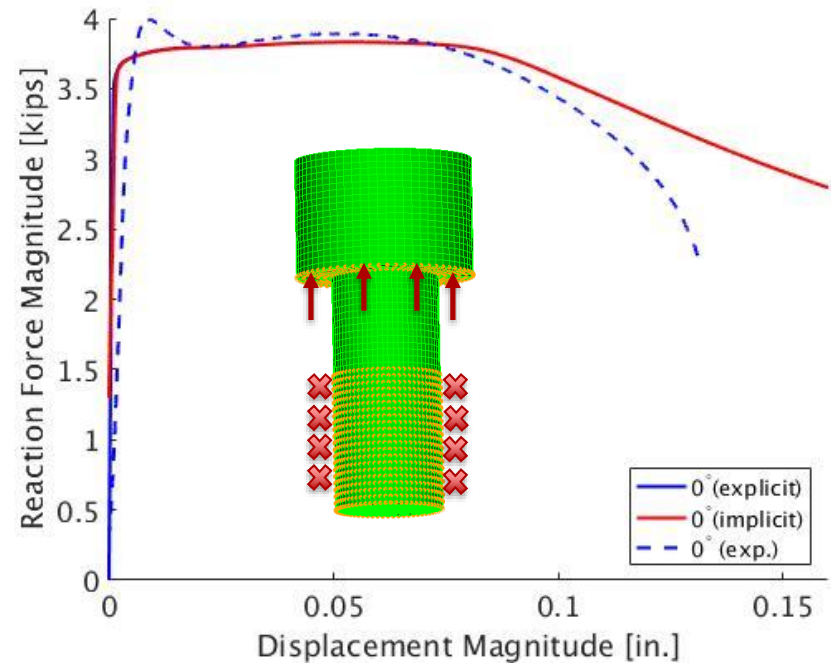


$$\theta_P = \arctan\left(\frac{P_x}{P_z}\right)$$
$$P_{\vec{u}} = P \cos(\theta_u - \theta_P)$$

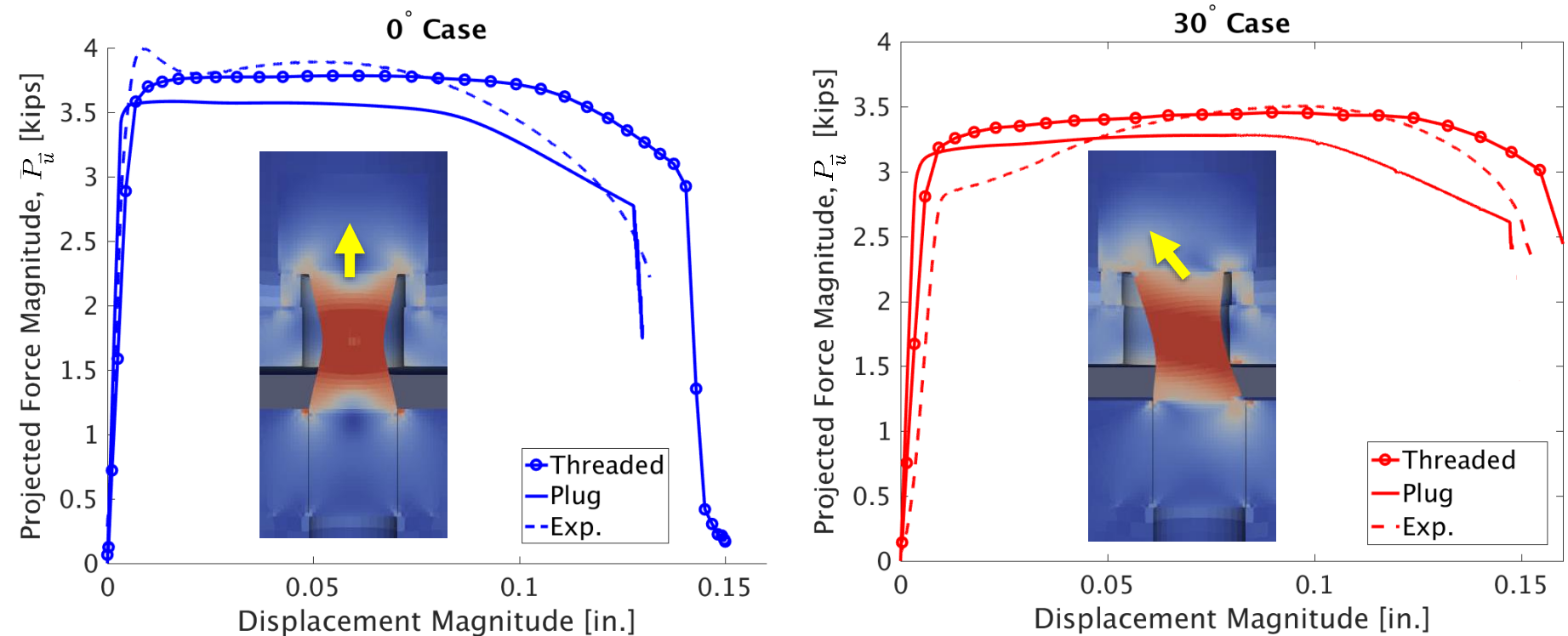
- Smoothing: moving average

Methodology: Numerical Procedures

- Implicit vs. Explicit
 - In order to account for the frictional contact between the plug and bushing an explicit model is required
 - For calibration purposes, the basic plug is analyzed using both implicit and explicit models
 - The hardening curve developed for the plug with bushing and threaded model are based on the this basic plug

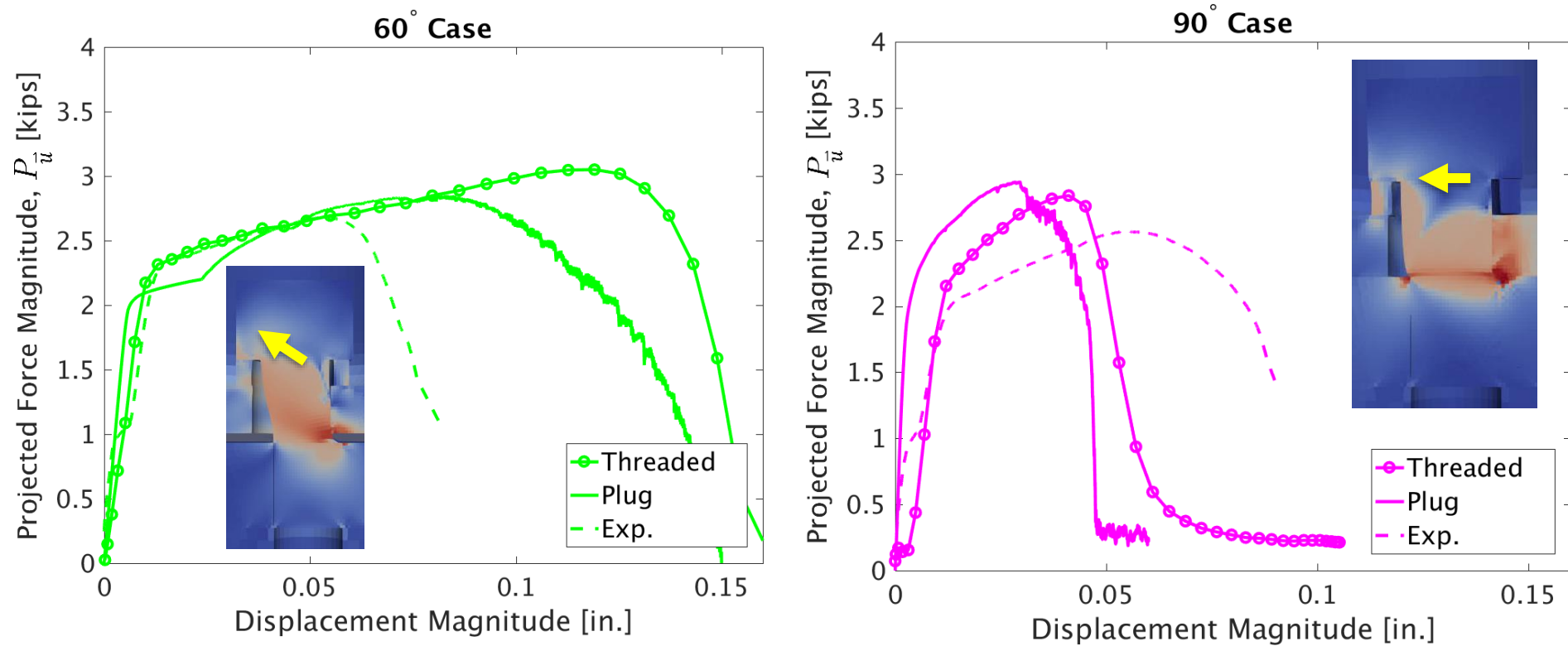


Results: FE vs. Experiments



- Element death on EQPS
- Plug model radius: tensile stress area

Results: FE vs. Experiments



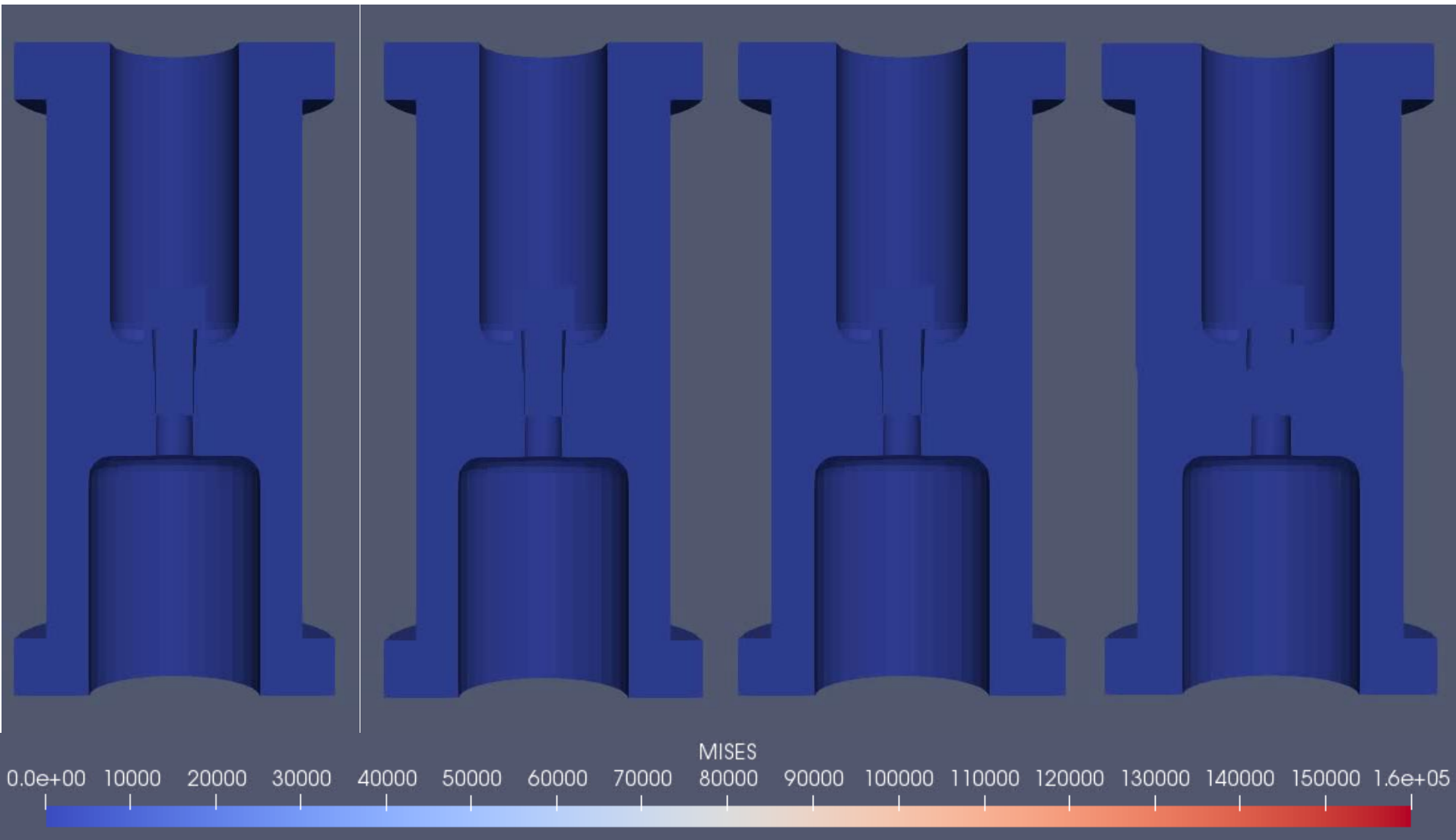
- Element death on EQPS
- Plug model radius: tensile stress area

0°

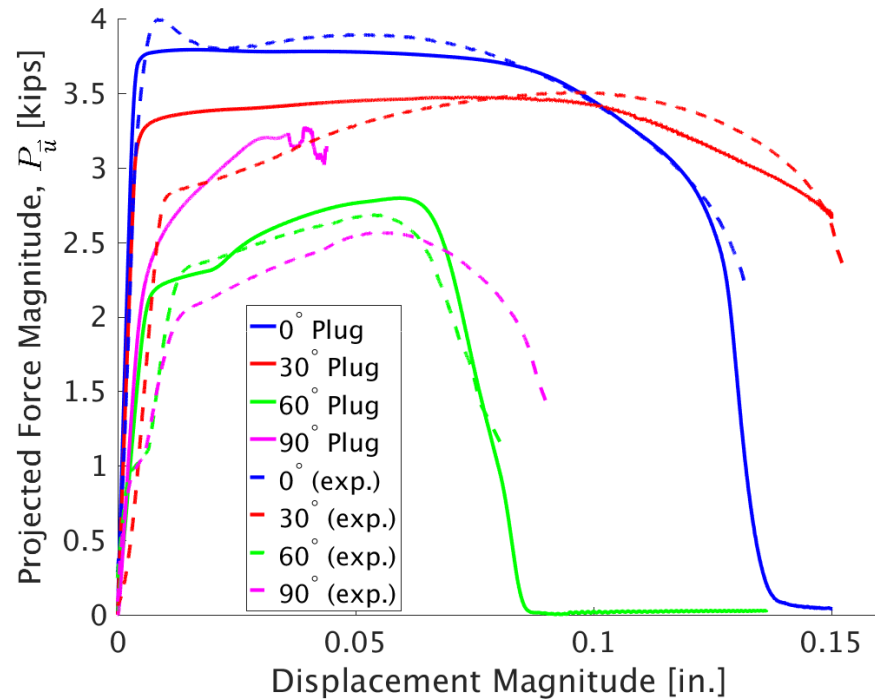
30°

60°

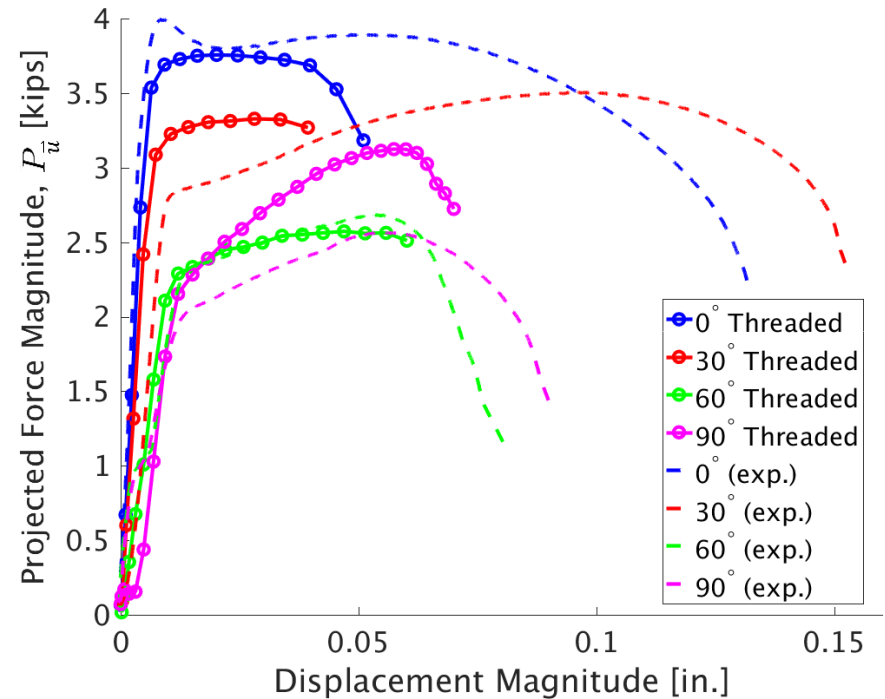
90°



Results: Ductile Damage Failure Model



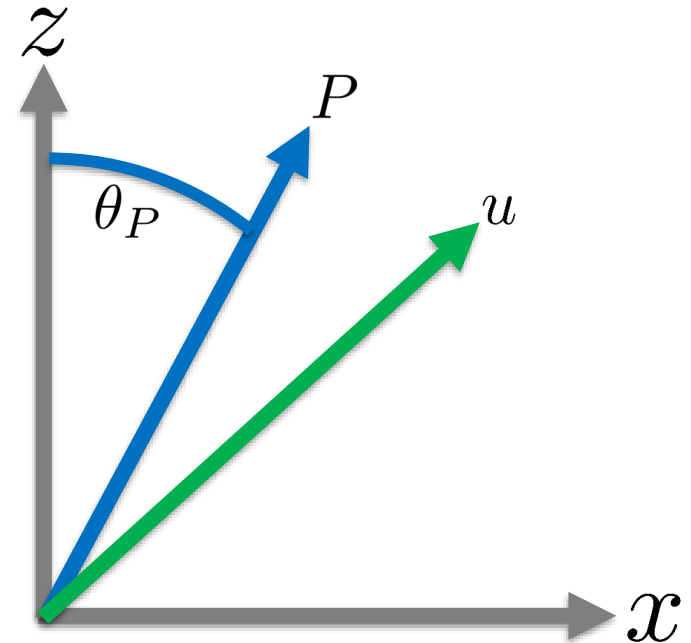
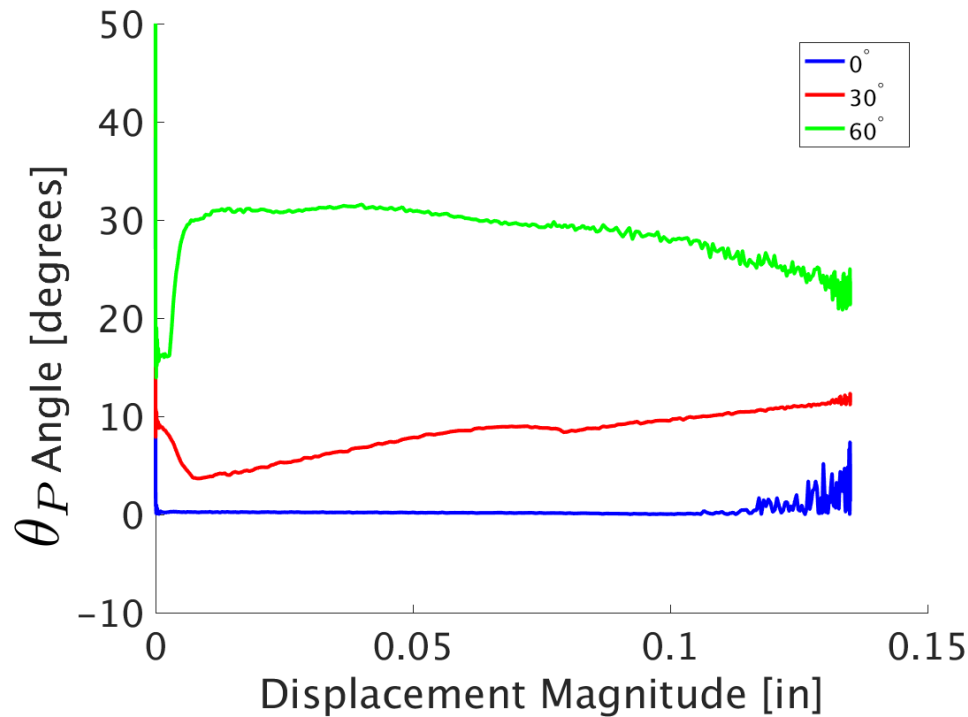
a) Plug Model



b) Threaded Model

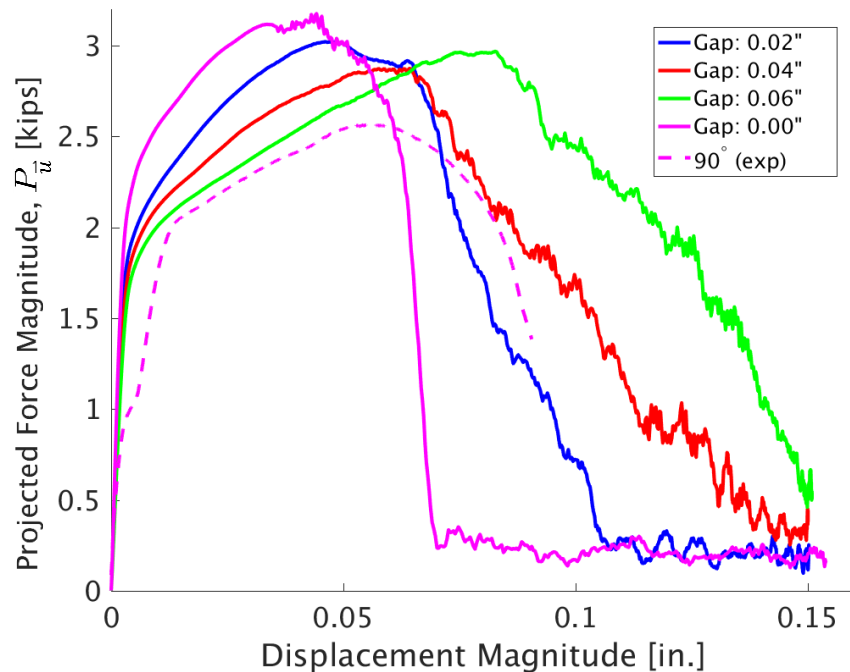
- ml_ep failure shown

Results: Load Angle vs. Displacement

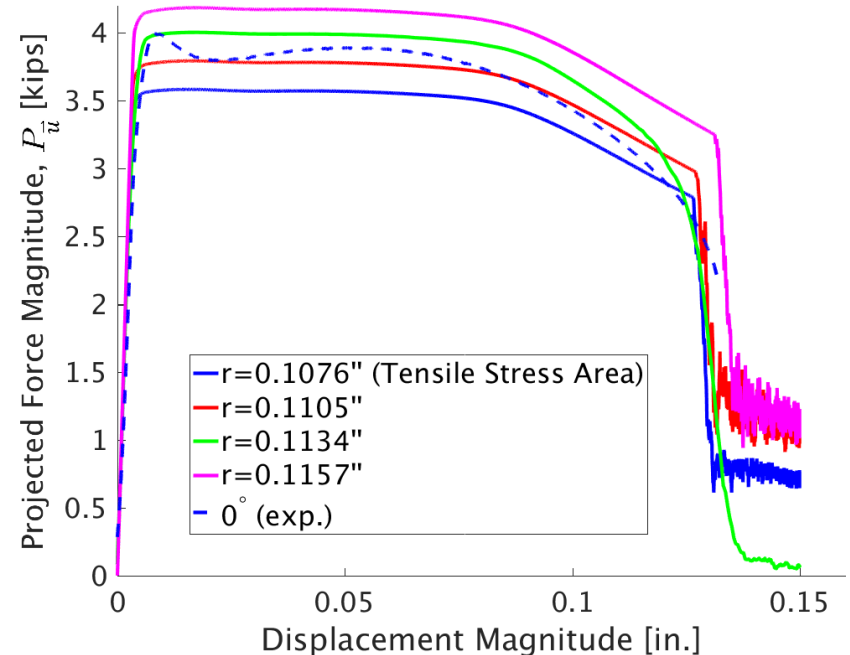


Results: Parameter Studies

- Various studies including: Effect of preload, friction, and yield stress



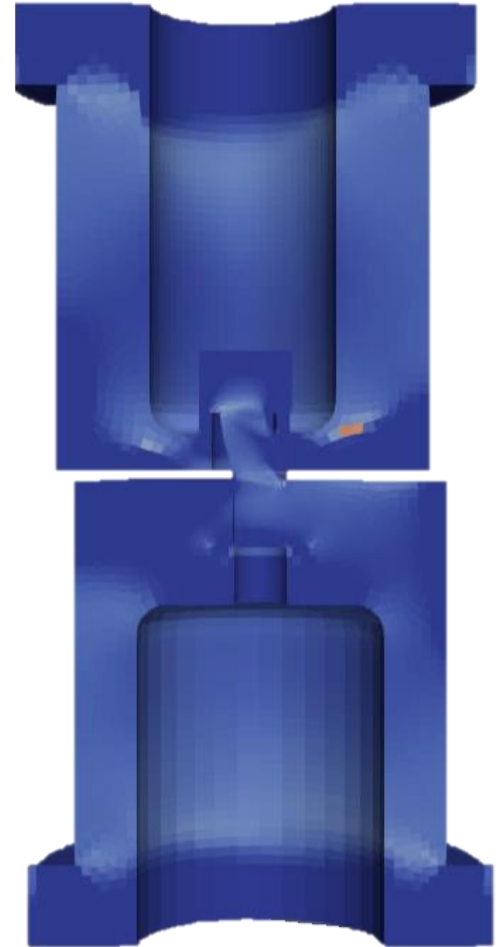
a) Initial bushing gap



b) Plug radius, r

Conclusion

- Plug model comparisons to:
 - Experiment data
 - A fully threaded FE model
- Research answers:
 - Plug models compare favorably for overall load-displacement behavior
 - Agreements to experiments were possible when load projection was considered
 - The failure models considered do not fully capture trends presented in experimental data



Mentor Team

Sandia National Laboratories

Jeffrey Smith

Peter Grimmer

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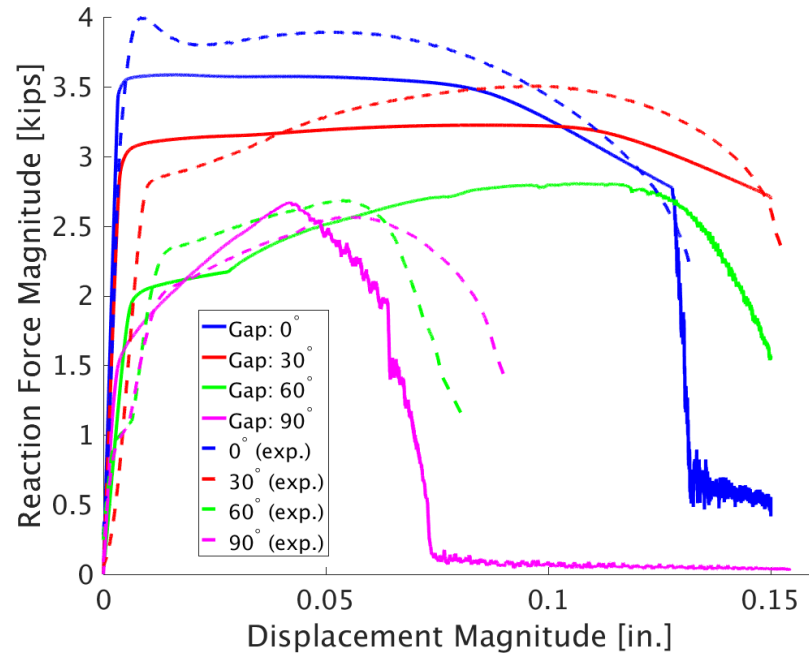
Cranfield University, UK

Gustavo Castelluccio

Acknowledgments

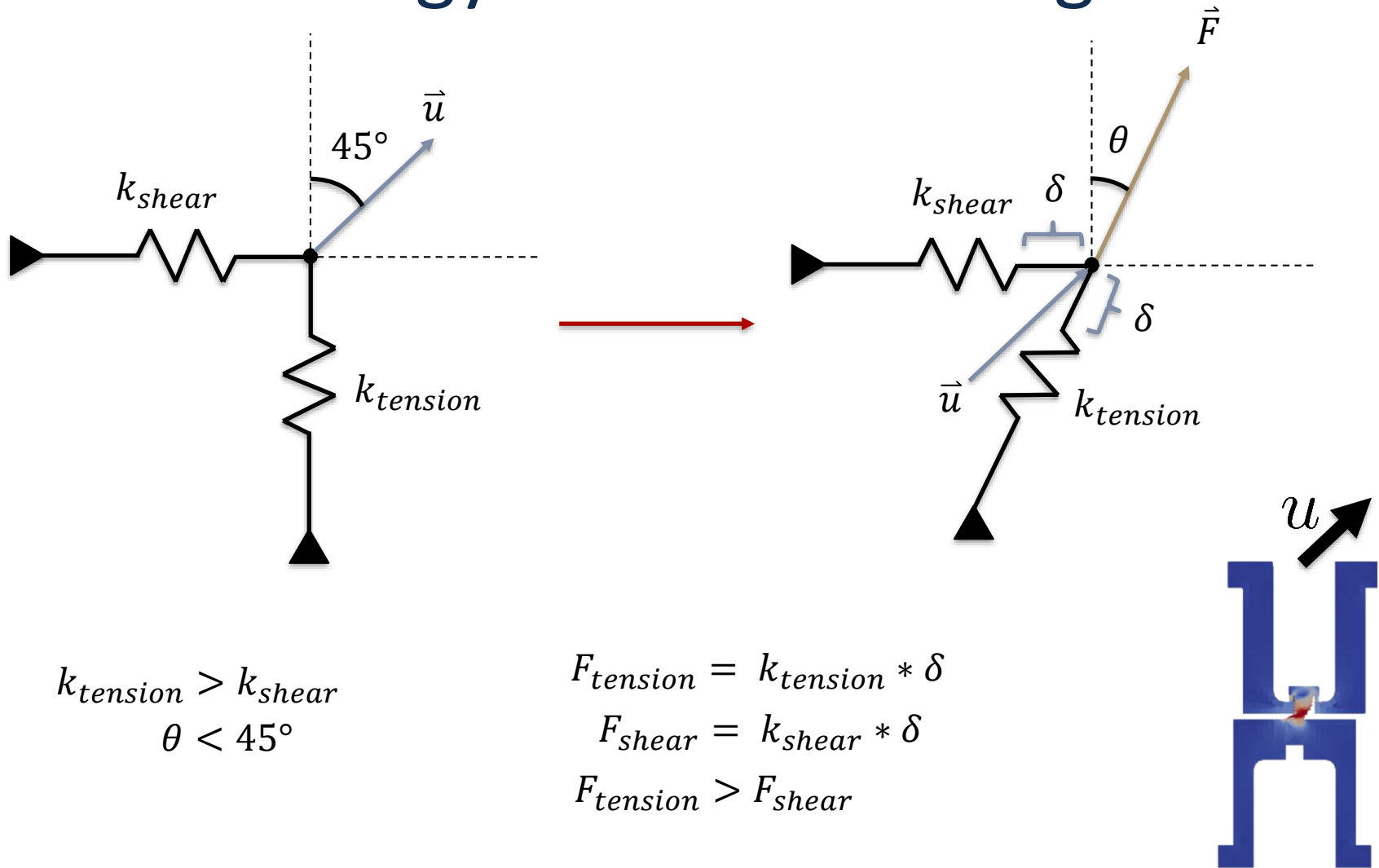
- This research was conducted at the 2018 Nonlinear Mechanics and Dynamics Research Institute hosted by Sandia National Laboratories and the University of New Mexico.
- Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA-0003525.

Backup Slides



a) Plug model with initial gap of 0.04"

Methodology: Post-Processing



Backup Slides

- Von Mises Yield Criterion:

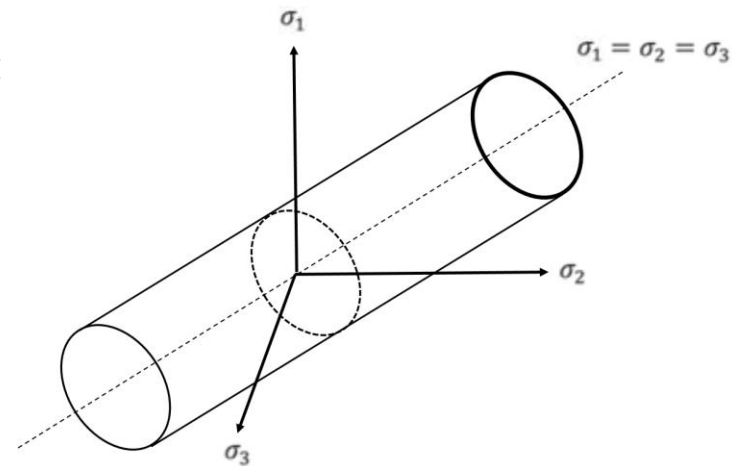
$$\sigma_{vm} = \sqrt{\frac{1}{2}[(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2]}$$

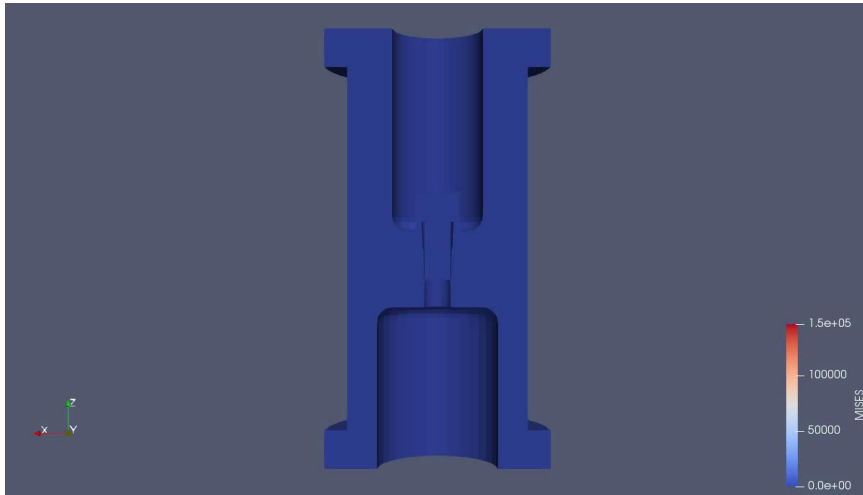
(Where $\sigma_{1,2,3}$ are the principal stresses, respectively)

- This defines a cylindrical 3D yield surface in principal stress space.
 - Axis is along hydrostatic stress states

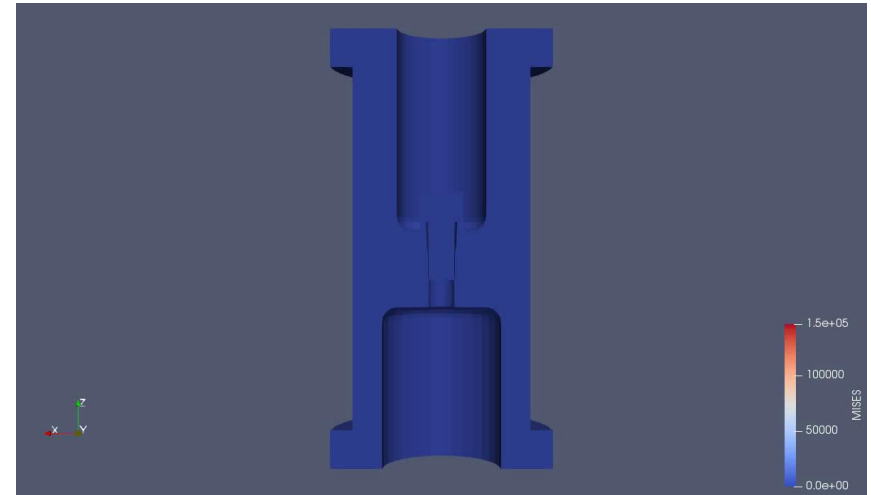
- σ_{vm} comes from deviatoric stress S :

$$\sigma_{ij} = S_{ij} + \frac{1}{3}\sigma_{kk}\delta_{ij}$$
$$J_2 = \frac{1}{2}S_{ij}S_{ij}$$
$$\sigma_{vm} = \sqrt{3J_2}$$

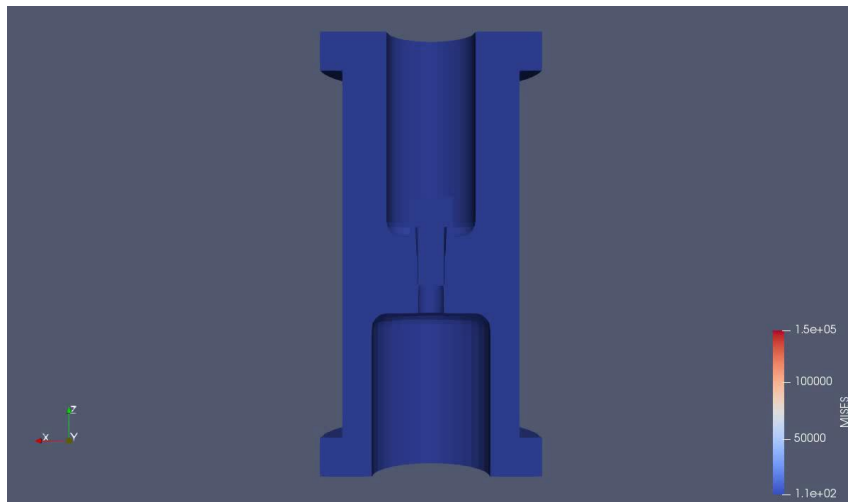




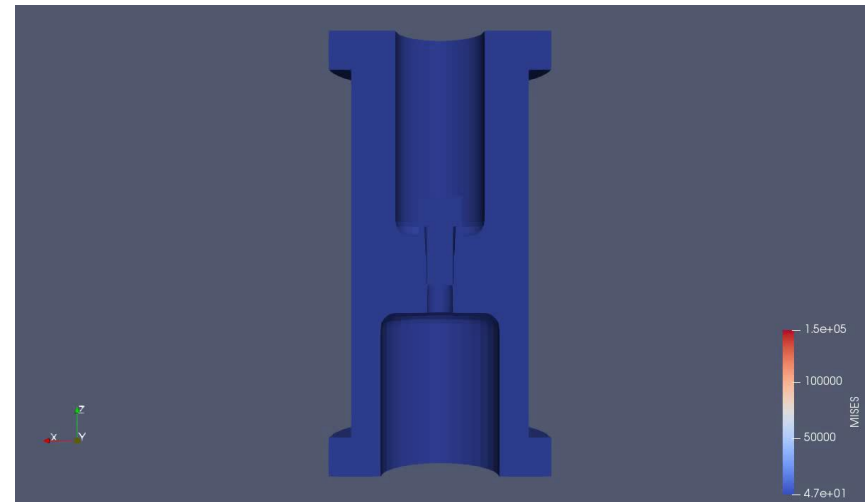
0-deg



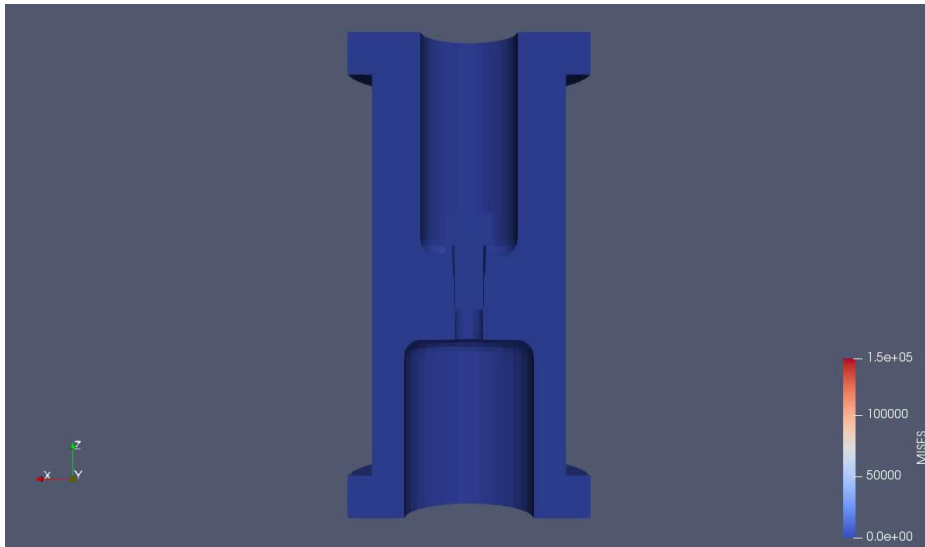
0-deg with tear



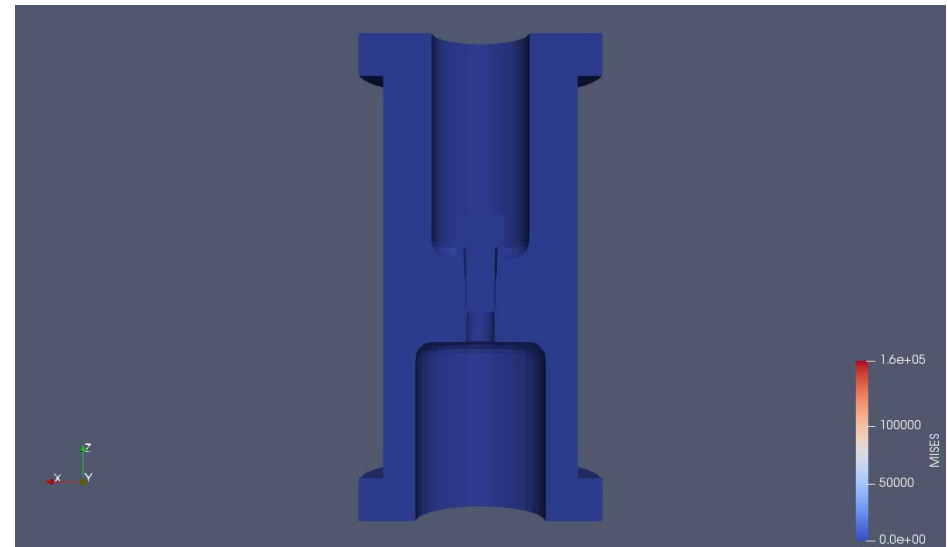
30-deg



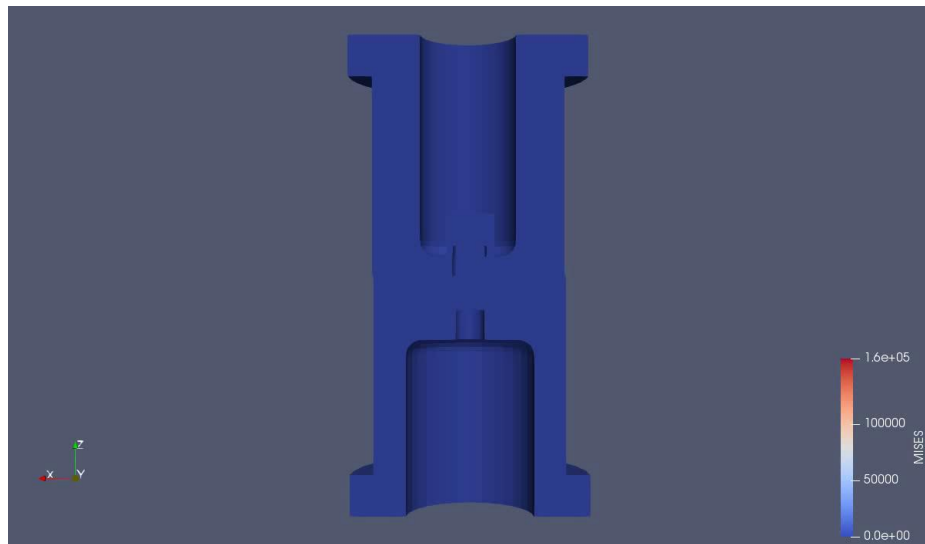
30-deg with tear



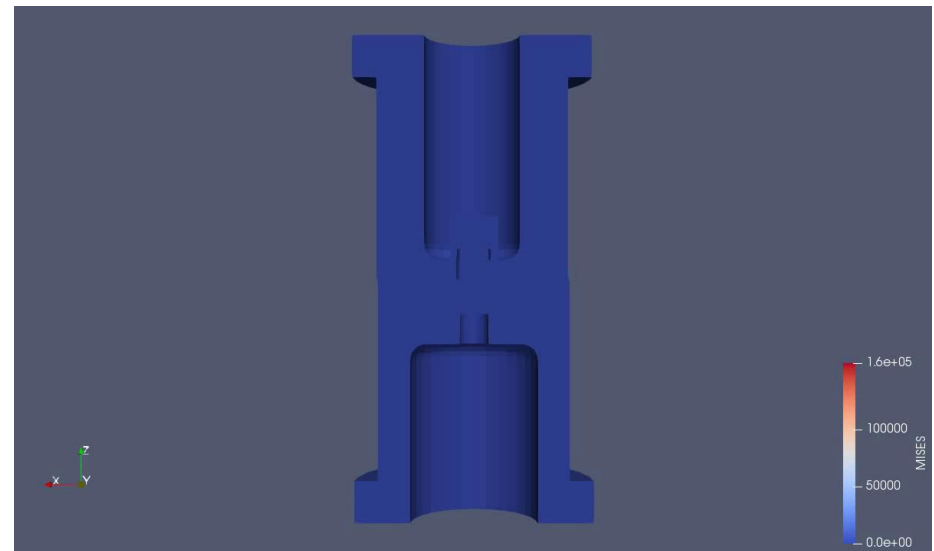
60-deg



60-deg with tear



90-deg



90-deg with tear

0-deg with tear

30-deg with tear

60-deg with tear

90-deg with tear

